

Analytical Model for Heterogeneous Crystallization Kinetics of Spherical Glass Particles

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An analytical model developed to describe the crystallization kinetics of spherical glass particles has been derived in this work. A continuous phase transition from three-dimensional (3D)-like to 1D-like crystal growth has been considered and a procedure for the quantitative evaluation of the critical time for this 3D–1D transition is proposed. This model also allows straightforward determination of the density of surface nucleation sites on glass powders using differential scanning calorimetry data obtained under different thermal conditions.

I. Introduction

IMPORTANT surface crystallization related phenomena, such as the vitrification ability of some supercooled liquids and the kinetic competition between viscous flow sintering and surface crystallization of glass powders,^{1,2} are commonly calculated by using an estimated number of heterogeneous nucleation sites per unit surface, $N_s = n/(NS_g)$. In this equation, it is assumed that a number N of equal-size glass particles each having surface area, S_g , can be formed with a total number of crystallization sites, n . However, there is no unambiguous and simple method to determine N_s from direct measurements³ on small glass particles. The value of N_s , the average particle radius, R , size distribution and the linear growth rate, u , determine the particle crystallization kinetics.^{4–7} In this article, we derived a model to account for the nucleation and growth of crystals of simple geometry on spherical glass particles. This modeling is based on the use of universal parameters and enables a simulation of the crystallization process and all its stages, which vary from three-dimensional (3D) growth on a glass particle surface to 1D growth toward its interior.

II. Theoretical Model

In order to characterize the crystallization of glass particles as a function of annealing time, t , we assume the most common case of heterogeneous nucleation of cylindrical crystals growing at a linear rate, u , from a fixed number of sites per unit area, N_s . Such type of growth generally initiates on the surface of the glass grains, with the circular base growing at the particle surfaces, and the cylindrical axis growing perpendicular to the particles surface toward their interior. According to the Johnson–Mehl–

Avrami–Kolmogorov (JMAK) theory,^{8–10} the crystalline volume fraction of a packing of spherical glass particles of radius R can be given by³

$$\alpha_v(t, N_s) = 1 - \exp\left(-\frac{3\alpha_s(t, N_s)ut}{R}\right) \quad (1)$$

(the validity of the JMAK theory has been experimentally confirmed for heterogeneous surface nucleation for the limiting case of large number of nucleation sites¹¹).

Let us consider a sample with total volume, V_T , where the parameter $\alpha_v = V_c/V_T$ characterizes the fraction of V_T that has been crystallized, V_c is the total volume occupied by crystals, $\alpha_s = S_c/S_g$ is the fraction of crystallized surface, defined by the ratio between the crystallized area, S_c , and the glass particle surface, S_g . The crystals at the surface reduce the effective surface of the glass particles available for further crystallization. Again, according to the JMAK theory,¹² the crystallized surface fraction is given by

$$\alpha_s(t, N_s) = 1 - \exp(-\pi N_s u^2 t^2) \quad (2)$$

Let us now introduce the reduced parameters $\tau \equiv ut/R$ and $v_s \equiv 4\pi R^2 N_s$. Note that v_s is the absolute number of nucleation sites on the surface of a spherical glass particle. With these new parameters, Eqs. (1) and (2) can be rewritten as

$$\alpha_v(\tau, v_s) = 1 - \exp(-3\alpha_s(\tau, v_s)\tau) \quad (3)$$

and

$$\alpha_s(\tau, v_s) = 1 - \exp\left(-\frac{v_s \tau^2}{4}\right) \quad (4)$$

respectively. Thus, the whole kinetic process depends only on dimensionless parameters. The surface and volume time-evolution of crystallization expressed in Eqs. (3) and (4) are universal because they do not explicitly depend on any specific glass composition or temperature. The above equations can be directly linked to differential scanning calorimetric (DSC) measurements.

It has been experimentally confirmed that the area under the DSC crystallization peak of partially crystallized samples, $A(\tau, v_s)$ (the filled contours in the left panels of Fig. 1) is proportional to the remaining glassy volume:

$$\alpha_g(\tau, v_s) V_T = (1 - \alpha_v(\tau, v_s)) V_T \quad (5)$$

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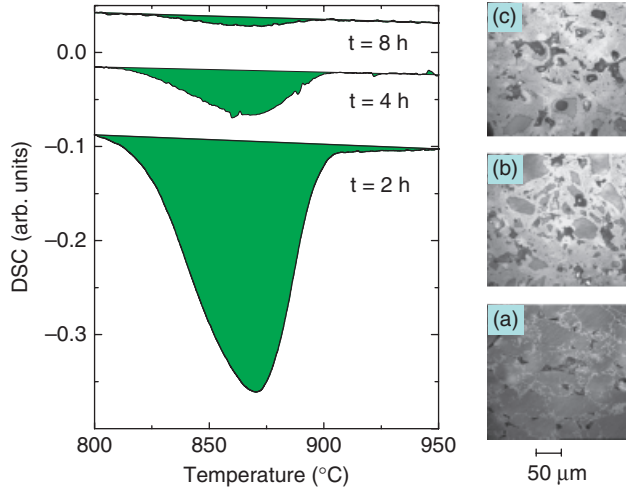


Fig. 1. Right: micrographs of polished sections of diopside glass particles sintered at 825°C for: (a) 2 h, (b) 4 h, and (c) 8 h. Color scale: light-gray phase, crystals; medium-dark gray phase, glass; from dark gray to black and eventually white in the center due to reflecting light, pores. Left: the corresponding DSC spectra of samples subjected to the different annealing steps at 825°C before the DSC runs.

where $\alpha_g(\tau, v_s)$ is the glass volume fraction in these samples. (E. B. Ferreira, unpublished data)^{13,14} Thus,

$$A(\tau, v_s) \propto V_T(1 - \alpha_v(\tau, v_s)) \quad (6)$$

The total volume can be expressed by the ratio between the sample mass, m , and the density of the solid material as

$$V_T(\tau) = \frac{m}{(\rho_g + \alpha_v(\tau, v_s)(\rho_c - \rho_g))} \quad (7)$$

where ρ_c and ρ_g are the mass densities of the crystal and glass phases, respectively. Now, considering equal-mass samples, it is possible to obtain the ratio between the area under a DSC crystallization peak, at any given time of the crystallization process, $A(\tau, v_s)$, and the area at $t = 0$, $A(0, v_s)$ as

$$\frac{A(\tau, v_s)}{A(0, v_s)} = \left(1 + \frac{\alpha_v(\tau, v_s)}{(1 - \alpha_v(\tau, v_s))} \frac{\rho_c}{\rho_g}\right)^{-1} \quad (8)$$

Hence, this equation yields a universal pattern, establishing a direct relationship between the dimensionless parameters τ and v_s , and the ratio between mass densities, ρ_c/ρ_g .

III. Results and Discussion

In Fig. 1 we show an example of sequential crystal growth steps during the sintering of diopside ($\text{CaO} \cdot \text{MgO} \cdot 2\text{SiO}_2$) glass powders. The micrographs correspond to annealing steps performed at 825°C for 2 h (a), 4 h (b), and 8 h (c). After 2 h of thermal treatment, crystal formation can be detected around the vitreous grains, shown by light dots in Fig. 1(a). After impingement of the crystals on the surface of the glass grains (Fig. 1(b)), 1D growth prevails, ($t > 4$ h). This process finally leads to the complete transformation of the former vitreous phase into crystals that grow from the surface toward the grain interior (Fig. 1(c)). These samples were further characterized by DSC, as shown by the corresponding graphics on the left-hand side of Fig. 1.

In Fig. 2(a), the function $A(\tau, v_s)/A(0, v_s)$ is displayed for different values of v_s , for the ratio $\rho_c/\rho_g = 1.162$, where $\rho_c = 3261 \text{ kg/m}^3$ and $\rho_g = 2805 \text{ kg/m}^3$ (diopside parameters). One can note in this figure the agreement with experimental

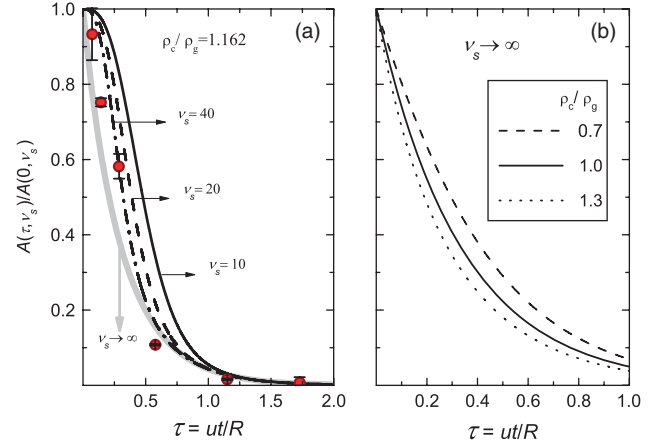


Fig. 2. (a) Plot of $A(\tau, v_s)/A(0, v_s)$ for $\rho_c/\rho_g = 1.162$ and different values of the universal parameter v_s . The limiting case, $v_s \rightarrow \infty$ is indicated by the thick gray solid curve. Circles: experimental points taken from DSC spectra of diopside samples. (b) Plot of $A(\tau, v_s)/A(0, v_s)$, in the limiting case $v_s \rightarrow \infty$, for a few values of the ratio ρ_c/ρ_g .

points obtained from DSC (some are displayed in Fig. 1), where the nominal values $u = 2 \times 10^{-10} \text{ m/s}$ and $R = 5 \mu\text{m}$ were used to obtain the dimensionless parameter τ . For large values of N_s and v_s , the crystallization process can be characterized as 1D growth. Such crystal growth conditions are often observed, as shown for example in Fig. 1(b) and (c) for diopside glass samples annealed at 825°C for over 4 h, where the surface of the original glass particles is totally crystallized. In the limiting case of large N_s or, according to Eqs. (3) and (4), for $v_s \rightarrow \infty$, the value of the crystalline volume fraction becomes

$$\alpha_v(\tau, \infty) = 1 - \exp(-3\tau) \quad (9)$$

The corresponding values of $A(\tau, \infty)/A(0, \infty)$, for $\rho_c/\rho_g = 1.162$, have been indicated in Fig. 2(a) by a thick solid gray curve. They determine the lowest limit of $A(\tau, v_s)/A(0, v_s)$, for any possible combination of parameters. The dependence on the density ratio ρ_c/ρ_g can be seen in Fig. 2(b), by setting $v_s \rightarrow \infty$ within the interval $\rho_c/\rho_g \in [0.7, 1.3]$. Thus, the volume fraction $\alpha_v(\tau, v_s)$ can be expressed as a function of the area and mass density ratios, $A(\tau, v_s)/A(0, v_s)$, and ρ_c/ρ_g , after using Eq. (8), in the form

$$\alpha_v(\tau, v_s) = \left(1 + \frac{A(\tau, v_s)/A(0, v_s)}{(1 - A(\tau, v_s)/A(0, v_s))} \frac{\rho_c}{\rho_g}\right)^{-1} \quad (10)$$

One should note that simple DSC measurements performed with two samples with the same mass, a partially crystallized and a glassy one, provide the crystallized volume fraction $\alpha_v(\tau, v_s)$ of materials with known density ratio ρ_c/ρ_g . One obtains $\alpha_v(\tau, v_s)$ from Eq. (10) and by knowing u and R , together with Eqs. (3) and (4), one can find the value of the universal parameter v_s as

$$v_s = -\frac{4}{\tau^2} \ln\left(1 + \frac{1}{3\tau} \ln(1 - \alpha_v(\tau, v_s))\right) \quad (11)$$

Equations (10) and (11) show that experimental values of $A(\tau, v_s)/A(0, v_s)$ for any τ and ρ_c/ρ_g determine the universal parameter v_s . Consequently, the experimental value for R determines the number of heterogeneous nucleation sites per unit surface, N_s .

As mentioned before, this surface crystallization process can be divided in two main steps, each one with a predominant morphological characteristic: (i) 3D-like crystal growth on the surface and into the interior of glass particles, (ii) when the total surface

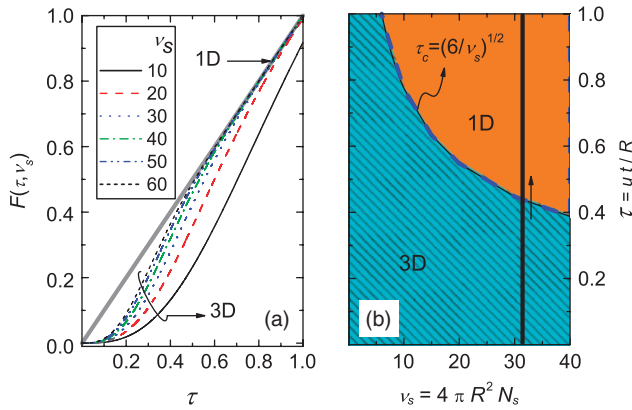


Fig. 3. (a) Function $F(\tau, v_s)$ for various values of v_s (the asymptotic limit $F(\tau, v_s) \rightarrow \tau$ that corresponds to the 1D growth mode is shown). (b) Regions of predominant 1D and 3D modes of crystal growth highlighted in continuous and striped patterns, respectively. Dashed curve: calculated critical parameter τ_c , as a function of v_s . Solid vertical line: path corresponding to experimental observations shown in Fig. 1.

area of the glass particle is filled with crystals ($\alpha_s(\tau, v_s) \rightarrow 1$), the crystal layer continues to grow toward the glass interior in a 1D mode. However, our model allows one to characterize this continuous 3D–1D transition in terms of effective parameters and critical values. We can introduce the function

$$F(\tau, v_s) \equiv \frac{1}{3} \ln(1 - \alpha_v(\tau, v_s))^{-1} = \alpha_s(\tau, v_s) \tau \quad (12)$$

The 3D-like crystal growth is halted when $\alpha_s(\tau, v_s) \rightarrow 1$ and this condition corresponds to the asymptotic limit $F(\tau, v_s) \rightarrow \tau$. In Fig. 3(a), we show the plots of $F(\tau, v_s)$ for different values of v_s . In order to reach a criterion for the characterization of the transition between the two crystallization modes, we can define a critical dimensionless time, τ_c , where $d^2F(\tau_c)/d\tau^2 = 0$. This yields an exact value of the critical dimensionless time for the 3D–1D phase transition between the crystallization growth modes given by $\tau_c = \sqrt{6/v_s}$ (depicted in Fig. 3(b)). It is important to note that this criterion gives, according to Eq. (4), the boundary value for the crystallized surface fraction

$$\alpha_s(\tau, v_s) = 1 - \exp\left(-\frac{6}{4}\right) \cong 0.7769$$

which is independent of v_s . In terms of the critical dimensionless time, Eq. (4) transforms to

$$\alpha_s(\tau, v_s) = 1 - \exp\left(-\frac{6}{4} \left(\frac{\tau}{\tau_c}\right)^2\right) \quad (13)$$

A universal phase diagram can be produced, as shown in Fig. 3(b), which depends only on τ and v_s and such a diagram may be used to characterize the crystallization process of spherical glass particles. This is a relevant factor in problems, such as in the control of viscous sintering with concurrent surface crystallization and of the residual porosity in sintered glasses. In the present case, DSC experiments yield a mean value $v_s \sim 30.4$. According to Eq. (11), this corresponds to $N_s \sim 1.2 \times 10^{11} \text{ m}^{-2}$ (the approximate experimental path during the thermal annealing is displayed in Fig. 3(b)). Given that $\tau_c = \sqrt{6/v_s}$ the value of the

critical dimensionless time for diopside yields $\tau_c = 0.437$, that corresponds to 3 h of annealing (note that $\tau \equiv ut/R$), in accordance with the micrographs in Fig. 1.

IV. Conclusions

We developed a universal mathematical treatment to deal with the crystallization kinetics of spherical glass particles. Our model has no boundary when passing from the 3D-like crystallization mode on the surface to a 1D-like mode toward the glass interior. We have shown how the area under DSC crystallization peaks of two samples, one partially crystallized and other glassy, can be used to determine important parameters, such as the number of heterogeneous nucleation sites per unit surface, and the crystallized volume fraction. Finally, we have proposed a phase diagram to characterize the crystallization process of spherical glass particles based on universal parameters.

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